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Practical Equivalent Control in 2-Sliding Controls Applied to an Anthropomorphic Robot Arm

Karim Braikia, Pascal Acco, Bertrand Tondu and Mourad Chettouh

Abstract—Driving an anthropomorphic robot arm driven by pneumatic artificial rubber muscles (PARMs) with a direct transmission is quite delicate. PARMs present complex nonlinearities and robust control tools are unavoidable. Among them, those applied are the *twisting* and *super twisting* algorithms, which belong to the 2-higher order sliding mode control set. In this paper it is studied the effect of the equivalent control in sliding mode controller based on variable structure systems (VSS) theory. It will be shown when to use the equivalent control, and the effects of a noisy sensor signal on control performance. Experimental results are presented and discussed.

I. INTRODUCTION

Driving a robot manipulator with direct transmission is a difficult task, mainly because of coupling effect, gravity, payload variation and actuator characteristics. The PARMs have some good properties [4] such as lightweight and low price. They also present compliance and bio mimetic properties. This compliance is of great interest when such an arm is used in human shared environments. There is renewed interest for flexible manipulators driven by PARMs in several applications [5]. Nevertheless, a PARM present complex nonlinearities. Its force generation is nonlinear and it is subject to hysteresis [6] [7] and [8]. Artificial muscle characteristics vary with an increasing duty cycle [9], airflow properties and servo valves add to nonlinearities, see [10] for more details. A PARM is thus a naturally high nonlinear actuator and is difficult to model. The applied control technique must fulfil two necessities:

- Avoid both a complex model and a complex controller, which are not practical
- Robustness of the manipulator control against unknown parameters variations and modelling approximation

Control under heavy uncertainty conditions remains one of the main subjects of modern control theory. The sliding mode control (SMC) approach requirement is robustness against modelling errors. The idea is to introduce a new dynamic by imposing a switching surface. When sliding is reached, the system will become insensitive to parameter variations, modelling error and matched disturbances. These properties are very powerful tool in realizing a practical controller for either Single Input Single Output (SISO) or Multi Input Multi Output (MIMO) systems. The SMC allows the consideration of the mutual interaction of the joints

of robot as a disturbance and the definition of each joint of the manipulator as a SISO system. However the main drawback of standard SMC is mainly related to the *chattering effect* caused by the high-frequency control switching [11]. Chattering effect can deteriorate physical components and excite high frequency dynamics [12].

To overcome the above difficulties, the first idea is to add an equivalent control of a classical form of the SMC [13] and [14]. The other approach is to introduce higher order sliding mode in order to reduce chattering [15] and [16] while increasing accuracy in sliding [17]. Although control can be satisfied without the use of the equivalent control [18]. The usual control based on sliding mode is the sum of both controls: equivalent and sliding discontinuous control [13] and [14].

In the following, two well known 2-sliding control laws are studied: the *twisting* and *super twisting* algorithms [19], [20], [21], and [17]. The effect of equivalent control on regulation performance under heavy uncertainty will be shown. Its use in some cases is beneficial and can in others lead to performance degradation. It will also be shown when to use this equivalent control. Furthermore, the effect of a noised sensor signal on control performance is also addressed.

The paper is organized as follows: first the experimental set up is presented together with the actuator, the model identification is presented in section II. Then, the two 2-sliding algorithms previously indicated are established. Analysis of the use of the equivalent control and the effect of a noisy sensor signal on 2-sliding algorithms then follow. Finally, results are discussed and conclusions drawn.

II. ROBOT AND ACTUATOR

The control approach described in this paper has been tested on the anthropomorphic robot arm (Fig.1). Located at the Departement of Electrical Engineering of INSA de Toulouse. It consist of 7 degrees of freedom (d.o.f), each joint is driven by a pair of PARMs [7] [8], assembled in an antagonistic posture, through the application of a pressure variation ΔP upon an initial pressure P_0 (Fig.2). The torque generated by a pair of PARMs may be written as:

$$\Gamma = A(k_1\Delta P - k_2\theta) \quad (1)$$

A , k_1 and k_2 are constant parameters depending on muscle geometry [8]. The first term of (1) is the driving component proportional to pressure variation ΔP , while the second one is the restoring torque of a spring like stiffness Ak_2 , which actually is the compliance term where θ represents

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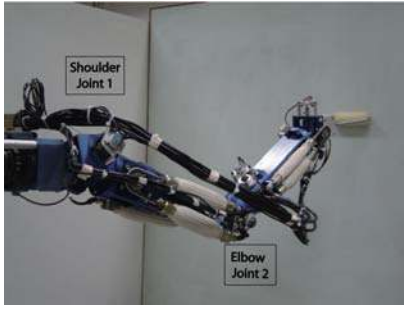


Fig. 1. The 7 d.o.f flexible robot arm

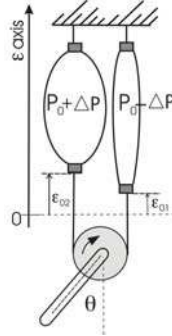


Fig. 2. Two PARMs in antagonistic posture

the angular displacement. It is worth noting that the system is open loop stable.

There are, on each joint, analog resistive sensors but no pressure sensors to monitor internal muscle pressure. The Intensity/Pressure (I/P) converter is supposed to be linear, which is not always true [22]. The PARMs used are developed within the LATTIS robotics laboratory at INSA Toulouse.

A. Model synthesis

In this application, two regional joints are controlled in regulation: Joint 1 (shoulder) and Joint 2 (elbow). The dynamic description based on generalized forces is:

$$J\ddot{\theta} + h(\theta, \dot{\theta}) + g(\theta) = \Gamma(u, \theta, \dot{\theta}) \quad (2)$$

Where θ and $\dot{\theta}$ are respectively the angular position and velocity vectors, J is the inertia related matrix, $h(\theta, \dot{\theta})$ is the vector of centrifugal, coriolis, and friction terms. $g(\theta)$ is the vector of gravity terms and $\Gamma(u, \theta, \dot{\theta})$ is the torque input

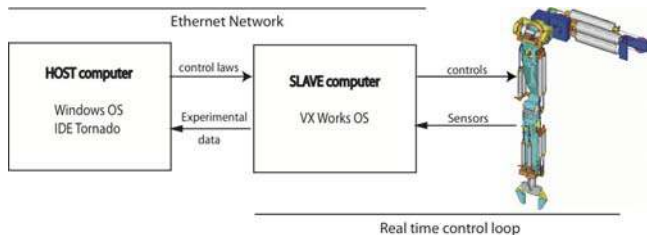


Fig. 3. Robot control architecture

vector, u is the control vector such that $\Delta P_i = f_p(u_i)$, where f_p represents the transfer function of I/P.

Identification is carried out in open loop without payload, control step variations are applied to both joints in order to bring out the existing coupling effect. Joint dynamics is based on the estimation of coefficients of a supposed linear model. Sliding mode enables the assumption of decoupled manipulator joint (SISO). The joints interaction may be regarded as an external perturbation. The best linear curve to a presumed SISO input/output data (u/θ) is obtained by using Idproc of Matlab. The two joints coefficients average values as well as their percentage variations are indicated in table I. The transfer function for a delayed joint is:

$$\frac{\theta_i}{u_i} = \frac{k_i}{1 + 2\zeta_i\tau_i s + \tau_i^2 s^2} \cdot e^{-t_i s}, \quad i = \{1, 2\} \quad (3)$$

TABLE I
AVERAGE MODEL PARAMETERS VALUES

parametres	joint 1	joint 2
k_i (rad/bar)	$0.31 \pm 7\%$	$0.48 \pm 40\%$
$\tilde{\tau}_i$ (s^{-1})	$0.16 \pm 10\%$	$0.10 \pm 39\%$
$\tilde{\zeta}_i$	$0.85 \pm 11\%$	$0.31 \pm 21\%$
\tilde{t}_i (s)	$0.18 \pm 26\%$	$0.06 \pm 31\%$

The resulting model coefficients variations estimations show that joint 2 is significantly influenced by the joint 1 dynamics, the opposite is not true. Model parameters variations separating a 0Kg from a 0.5Kg payload are indicated in table II. As it may be noted joint 2 is a lot more sensitive to payload variation (approximately 60 %) than joint 1. This strengthens the need to resort to robust control. Also, in the following, hysteresis is not considered, as only increasing pressure/response data was used and delay is also considered as included in the overall model uncertainties.

TABLE II
PARAMETERS VARIATIONS SEPARATING 0KG FROM 0.5KG PAYLOADS

parametres	joint 1	joint 2
\tilde{k}_i (rad/bar)	-4.83%	-9.14%
$\tilde{\tau}_i$ (s^{-1})	8.23%	-23.80%
$\tilde{\zeta}_i$	15.18%	233.91%
\tilde{t}_i (s)	8.53%	9.01 %
average variation	9%	68%

III. SECOND ORDER SLIDING MODES

The principle of sliding mode control is to get the state to reach and remain on a predefined function named sliding surface (σ) or manifold through discontinuous feedback [14] and [13]. Given a nonlinear system:

$$\begin{cases} \dot{x} = f(x, t) + g(x, t)u \\ y = \sigma(x, t) \end{cases} \quad (4)$$

$$\{x, f(x, t)\} \in \mathbb{R}^n, g(x, t) \in \mathbb{R}^{n \times m}, u \in \mathbb{R}^m$$

Where x is the state variable, t is time and u the control. $f(x,t)$ and $g(x,t)$ are smooth uncertain functions and $\sigma(x,t)$ the smooth output is the sliding function. The discontinuous control is:

$$u = \begin{cases} u^+ & \text{if } \sigma(x,t) < 0 \\ u^- & \text{if } \sigma(x,t) > 0 \end{cases} \quad (5)$$

This control law has proven its robustness versus system parameters variations, modelling uncertainties and matched perturbations. It, however, engenders chattering that can degrade performance and may even deteriorate physical components [14] and [12]. In order to attenuate chattering, High Order Sliding Modes (HOSM) controls have shown their capabilities by driving the chatter back onto the higher time derivatives of the sliding manifold [16], [17] and [14]. The actual control is the output of cascading integrators. This enables to keep the main advantages of classical 1-sliding and at the same time reduce chatter and increase sliding precision [17]. Given a constraint function $\sigma(x,t) = 0$, the r -sliding set is defined as:

$$\sigma_r = \{x \in \mathbb{R}^n \mid \sigma(x,t) = \dot{\sigma}(x,t) = \dots = \sigma^{(r-1)}(x,t) = 0\} \quad (6)$$

Moreover, in real sliding with a finite sampling time λ , sliding precision is up to the r th order with respect to λ , i.e. $|\sigma| = O(\lambda^r)$. Given, without loss of generality, a SISO nonlinear system:

$$\begin{cases} \dot{x} = f(x,u,t) \\ y = \sigma(x,t) \end{cases} \quad u = U(x,t) \in \mathbb{R} \quad (7)$$

$f(x,u,t)$ is a smooth uncertain function with $\frac{\partial}{\partial u} f(x,u,t) \neq 0$ and the smooth output is the sliding variable. If the sliding variable is chosen, as often, to be a first order dynamics:

$$\sigma_i(x,t) = c_i e_i + \dot{e}_i, \quad i = \{1, 2\} \quad (8)$$

Where $c_i > 0$ and $e_i = \theta_i - \theta_{d_i}$ is the error, the dynamics of system equation (7) satisfies a 2-sliding set equation (6).

With respect to $\sigma(x,t)$ if the Filippov set of state trajectories lie in the space tangential to the intersection of $\sigma(x,t) = 0$ and $\dot{\sigma}(x,t) = 0$ [23]. The relative degree of the considered system equation (3) with respect to $\sigma(x,t)$ is 1, as $\frac{\partial}{\partial u} \sigma(x,t) \neq 0$. Time derivation of $\sigma(x,t)$ yield:

$$\begin{aligned} \ddot{\sigma} &= \zeta(x,t) + \psi(x,t)\dot{u}(t), \\ \zeta(x,t) &= \frac{\partial}{\partial t} \dot{\sigma}(x,t,u) + \frac{\partial}{\partial x} \dot{\sigma}(x,t,u)f(x,u,t) \\ \psi(x,t) &= \frac{\partial}{\partial u} \dot{\sigma}(x,t,u) \end{aligned} \quad (9)$$

The new discontinuous control is $v(t) = \dot{u}(t)$. Assuming the new control $v(t)$ is bounded by $v_m \in \mathbb{R}^+$, that $\zeta(x,t)$ and $\psi(x,t)$ are bounded uncertain functions with $\psi(x,t) \in \mathbb{R}^+$, then there exist positive constants K_m , K_M and C_0 such that:

$$0 < K_m \leq \psi(x,t) \leq K_M \quad \text{and} \quad |\zeta(x,t)| \leq C_0 \quad (10)$$

If local coordinates $(z_1, z_2)^T = (\sigma, \dot{\sigma})^T$ are considered, then the 2-sliding problem is actually a finite time stabilisation of the second order auxiliary system described by:

$$\begin{cases} \dot{z}_1 = z_2 \\ \dot{z}_2 = \zeta(x,t) + \psi(x,t)v(t) \end{cases} \quad (11)$$

Two control laws able to stabilise system equation (11) in finite time are the *twisting* [21] and *super twisting* [19] algorithms.

A. Twisting law

The *twisting* algorithm is given by:

$$v(t) = \begin{cases} -u & \text{if } |u| > U_M \\ -A_m \text{sign}(z_1) & \text{if } z_1 z_2 \leq 0, \text{ and } |u| \leq U_M \\ -A_M \text{sign}(z_1) & \text{if } z_1 z_2 > 0, \text{ and } |u| \leq U_M \end{cases} \quad (12)$$

Where U_M is the bound of the effective control applied to the system and the sufficient conditions for finite time convergence are:

$$0 < A_m < A_M, \quad A_m > \frac{C_0}{K_m}, \quad K_m A_M - C_0 > K_M A_m + C_0$$

The applied control is thus: $u_{tw} = \int v(t)dt$

B. Super twisting law

The *super twisting* algorithm is a superposition of two components:

$$\begin{aligned} u_{stw} &= \int \dot{u}_1(t)dt + u_2(t) \\ \dot{u}_1 &= \begin{cases} -u & \text{if } |u| > U_M \\ -w \text{sign}(z_1) & \text{if } |u| \leq U_M \end{cases} \\ u_2 &= \begin{cases} -\alpha \varepsilon_0^\rho \text{sign}(z_1) & \text{if } |z_1| > \varepsilon_0 \\ -\alpha |z_1|^\rho \text{sign}(z_1) & \text{if } |z_1| \leq \varepsilon_0 \end{cases} \end{aligned} \quad (13)$$

Where U_M is the bound of the effective control applied to the system and $\varepsilon_0 > 0$ is the linearity bandwidth around the sliding surface σ . The sufficient conditions for finite time convergence are:

$$w > \frac{C_0}{K_m}, \quad \alpha^2 \geq \frac{4C_0 K_M (w + C_0)}{K_m^2 K_m (w - C_0)}, \quad 0 < \rho \leq 0.5 \quad (14)$$

C. Equivalent control in sliding mode

The control [14] and [13] is of the form:

$$u = u_{eq} + \Delta u \quad (15)$$

Where u_{eq} is a equivalent control, Δu is either *twisting* u_{tw} as defined in (12), *super twisting* u_{stw} as defined in (13).

The equivalent control, when ideal sliding is realised, will take the state trajectory to the equilibrium position. The effect of u_{eq} depends of the good estimation of the model parameters. However, it is unable to overcome in the system errors of modelisation and as it depends on the presumed model; if the latter is too far from the real model, it will induce undesirable performance.

The equivalent control can be written as:

$$u_{eq} = \tilde{u}_{eq} + \Delta u_{eq} \quad (16)$$

Where \tilde{u}_{eq} is the estimated equivalent control and Δu_{eq} represents the uncertainty in the equivalent control. Both quantities are linked to a presumed model and parameters uncertainties estimation. In order to compensate these uncertainties, the real control takes the form:

$$u = \tilde{u}_{eq} + \Delta u \quad (17)$$

Where \tilde{u}_{eq} represents a continuous low frequency component supposedly able to keep the state trajectory on the switching surface once it is reached, whereas Δu is a high frequency component able to ensure surface attraction despite uncertainties Δu_{eq} . In (17) Δu takes the forms of either the *twisting* or *super twisting* controls. If the uncertainties cannot be compensated by Δu , i.e. $-\Delta u_{eq} + \Delta u \neq 0$, convergence conditions (10) may not be satisfied.

twisting control (12) results in an integration of a discontinuous control. If *twisting* does not compensate model uncertainties in equation (17), the action Δu term loses its efficiency and convergence conditions (10) may not be satisfied.

Now, *super twisting* control (13) appears to be more interesting than *twisting* as it does not need to use $\dot{\sigma}(e, \dot{e})$; moreover, its control comprises a continuous term added to a discontinuous one. Again, if Δu does not compensate model uncertainties in equation (17), the action of the discontinuous term loses its efficiency and convergence conditions may not be satisfied. As shown in the next section.

IV. EFFECT OF NOISE ON CONTROL

Let us now consider a noised position sensor:

$$\theta_{\eta_i} = \theta_i + \eta \quad (18)$$

Where η is a white noise. Then sliding manifold σ_i may be rewritten as:

$$\sigma_i = c_i e_i + \dot{e}_i + (c_i \eta + \dot{\eta}), \quad e_i = \theta_i - \theta_{d_i} \quad (19)$$

The *twisting* control (12) is less sensitive to noise than the *super twisting* control as the integration attenuates chatter due to noise as well as smoothing the control. In the *super twisting* control (13), it is the discontinuous component $u_2(t)$ that may degrade performance.

$$u_2 = \begin{cases} -\alpha \varepsilon_0^\rho \text{sign}(z_1) & \text{if } |z_1| > \varepsilon_0 \\ -\alpha |z_1|^\rho \text{sign}(z_1) & \text{if } |z_1| \leq \varepsilon_0 \end{cases} \quad (20)$$

The presence of $\dot{\eta}$ in the expression of $z_1 = \sigma(e, \dot{e})$ may deteriorate performance, so the linearity bandwidth ε_0 has to be chosen small in order to avoid using $u_2(t) = -\alpha |z_1|^\rho \text{sign}(z_1)$. In which case, when outside ε_0 , the constant amplitude discontinuous action $u_2(t) = -\alpha \varepsilon_0^\rho \text{sign}(z_1)$ is of a classical form leading to chatter, unless α is small. Then, the action of the discontinuous part of the *super twisting* control, which was seen as an advantage over the *twisting* control will be attenuated. The remaining control (13) is then dominated by the continuous action $\int \dot{u}_1 dt$ leading to slow convergence and difficulty in compensating model uncertainties. Action of a noised sensor signal is depicted in the results section (section V).

V. EXPERIMENTAL RESULTS

A. Action of equivalent control

Combined shoulder and elbow are controlled in regulation with the reference vector $\Theta = (\theta_1, \theta_2) = (0.87, 1.04)^T \text{rad}$. With a 0.5Kg load attached to the end point which represents approximately 1/12 of the total mass of the robot arm. Each joint displacement is recorded to show the effect of \tilde{u}_{eq} using the *twisting* and *super twisting* laws. The switching surfaces are set as: $\sigma_1 = 12e_1 + \dot{e}_1$ and $\sigma_2 = 8e_2 + \dot{e}_2$. Parameters used in the regulation problem for the *twisting* law are found table III. Those used in the regulation problem for the *super twisting* law are stated in table IV.

Control laws used in this section are the following:

$$u = \varphi \tilde{u}_{eq} + \Delta u \quad (21)$$

with $\varphi = \{0, 25\%, 50\%, 75\%, 100\%\}$ and Δu is *twisting* or *super twisting*. As stated in section II-A, model coefficients variations of joint 1 are smaller than those of joint 2, the action of \tilde{u}_{eq} on joint 1 proves to increase performance, decreasing then rising and settling times, as depicted in Figs.4(a) and 5(a). However, it appears to destabilise joint 2 in both control laws as seen in Figs.4(b) and 5(b).

In Figs.4(a) and 5(a), joint 1 performance increases with increasing $\varphi \tilde{u}_{eq}$ while joint 2 becomes over-oscillating as seen in Figs 4(b) and 5(b). For joint 2, the attenuation factor φ is limited to 50% in order to preserve hardware integrity.

So, as model uncertainties of joint 2 are not be compensated by the control laws, convergence is not satisfied and the appropriate step in to avoid using \tilde{u}_{eq} . The equivalent control is only used for joint 1, totally, i.e. $\varphi = 1$.

B. regulation results

Control of joint 1 is of the form of (17). While joint 2, as the use of the equivalent control is rejected, control is established as:

$$u = \Delta u \quad (22)$$

Where Δu is either *twisting* or *super twisting* controls. Combined movements of both joints are controlled in regulation with two reference vectors to cover an operating range $[\Theta_1, \Theta_2]$ with $\Theta_1 = (0.69, 0.69)^T \text{rad}$ and $\Theta_2 =$

TABLE III

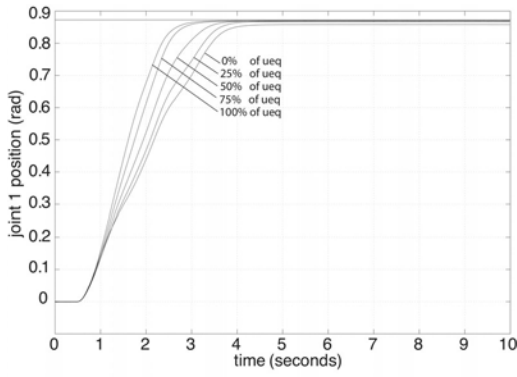
REGULATION PARAMETERS OF *twisting* LAW

Joint	shoulder (joint1)	elbow (joint2)
A_M	1.6	1.0
A_m	0.65	0.5
U_M	5	5

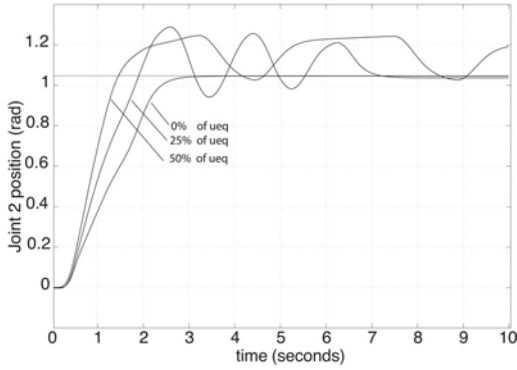
TABLE IV

REGULATION PARAMETERS OF *super twisting* LAW

Joint	shoulder (joint1)	elbow (joint2)
α	0.2	0.25
ε_0	0.2	0.2
W	1.5	0.95
U_M	5	5
ρ	0.5	0.5



(a) joint 1 (shoulder)



(b) joint 2 (elbow)

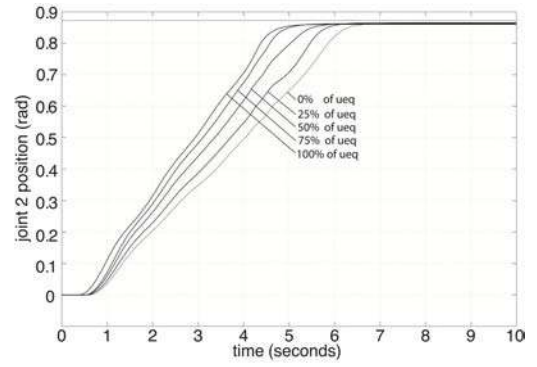
Fig. 4. Influence of \tilde{u}_{eq} with the *twisting* law and 0.5Kg load

$(0.87, 1.04)^T rad$ with payload variation. As it can be seen in Figs.6 and 7, both controllers can stabilize the system. Especially when equivalent control is not used on joint 2.

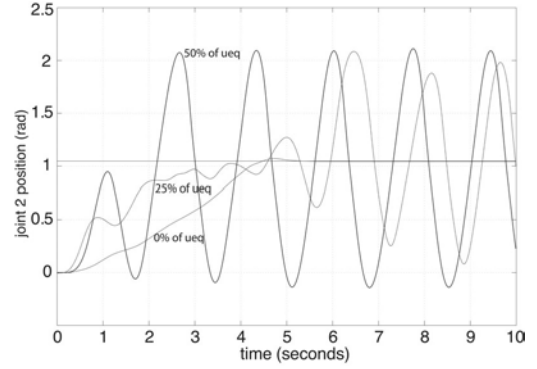
The reponse delay between *twisting* and *super twisting* is insignificant on joint 1. It should be noted that a delay of 0.75 s constant for almost all results presented, it is mainly due to: natural delay of the actuator as shown in section 2, and the I/P + airflow pipes. Without equivalent control on joint2 *twisting* reponse delay is more important compared *super twisting* controller (Figs.6 and 13). In all case it can be noted that settling time of *twisting* is better than *super twisting* on both joints of robot. in particularly with a payload of 0.5Kg.

Indeed, the sensor noise has limited the use of u_2 term in *super twisting* law. This performance has deteriorated, The remaining control (13) is then dominated by the continuous action $\int \dot{u}_1 dt$ leading to slow convergence and difficulty in compensating model uncertainties. This can be noted in Figs.8 and 9, for the *super twisting* law presented nearby sliding surface discontinuity.

The joint 2 is considered for the action of a perturbation which represents about 22% of the reference done under the controls of both *twisting* and *super twisting* laws. The reference $(0.87, 0.87)^T rad$ with a payload of 0.5 Kg is considered as one of the worst cases. The advantage of *twisting* over *super twisting* can again be noted before the

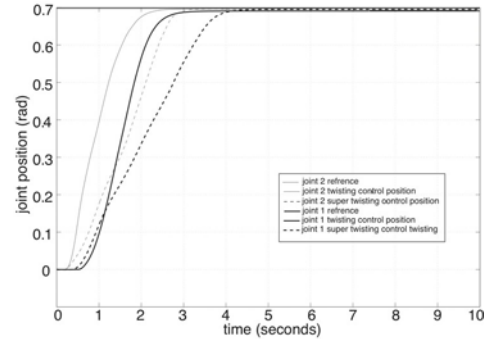


(a) joint 1 (shoulder)

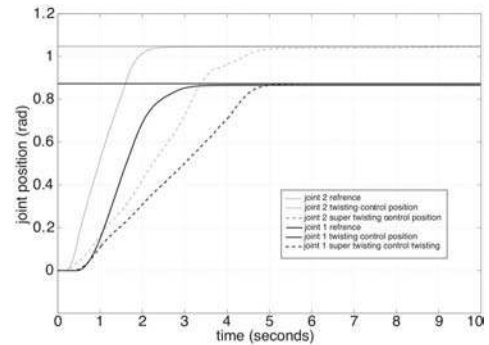


(b) joint 2 (elbow)

Fig. 5. Influence of \tilde{u}_{eq} with the *super twisting* law and 0.5kg load

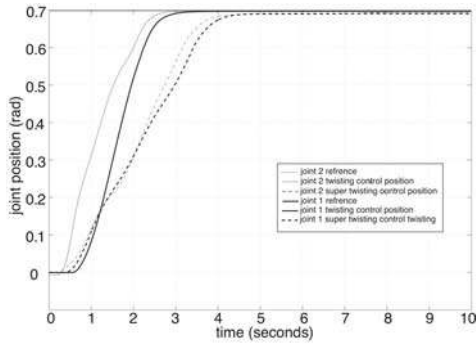


(a) $\Theta_1 = (0.69, 0.69)^T rad$

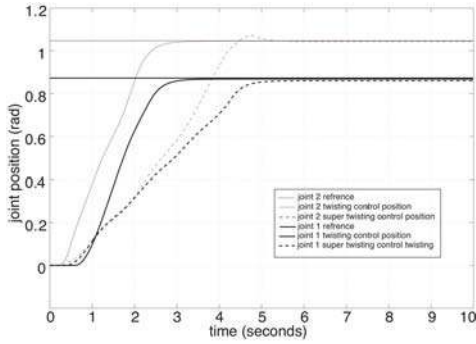


(b) $\Theta_2 = (0.87, 1.04)^T rad$

Fig. 6. regulation joint 1 and 2, *twisting* and *super twisting* laws (no payload)



(a) $\Theta_1 = (0.69, 0.69)^T \text{ rad}$



(b) $\Theta_2 = (0.87, 1.04)^T \text{ rad}$

Fig. 7. regulation joint 1 and 2, *twisting* and *super twisting* laws (0.5Kg payload)

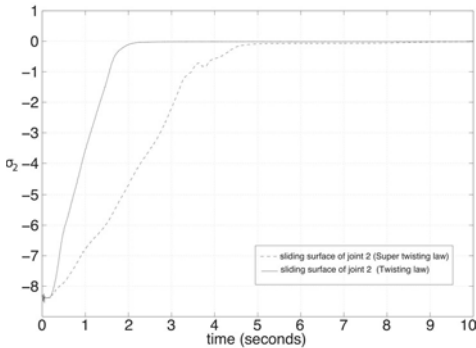


Fig. 8. sliding surface of Joint 2 *twisting* and *super twisting* laws (0.5Kg payload), $\Theta_2 = (0.87, 1.04)^T \text{ rad}$

action of the perturbation. Both laws succeed in restabilising the joints responses after the perturbation is applied. In the case of the *twisting* controller the first overshoot (after perturbation) is limited to 24 % of the reference whereas the overshoot of *super twisting* represents 58% of the reference, as you can see in Fig.10. It is noted that parameters of both controllers are kept the same as for the regulation problem (table III and IV).

C. Tracking a sinusoid

Let us now see the ability of the laws to make joint 2 track a sinusoid. Input trajectory is considered to be: $0.3491 \sin(2\pi ft) + 0.6981 \text{ rad}$, with 0.1 Hz frequency and a payload variation. The parameters of *twisting* and *super*

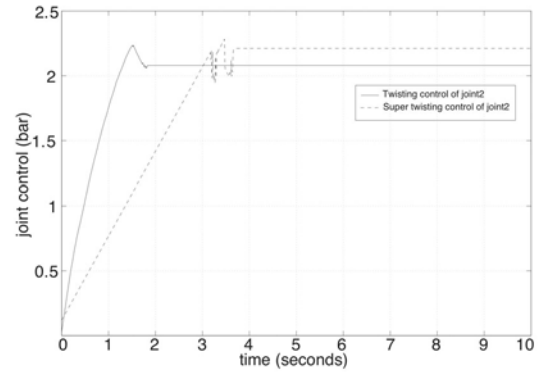


Fig. 9. *twisting* and *super twisting* laws (0.5Kg payload) joint 2, $\Theta_2 = (0.87, 1.04)^T \text{ rad}$

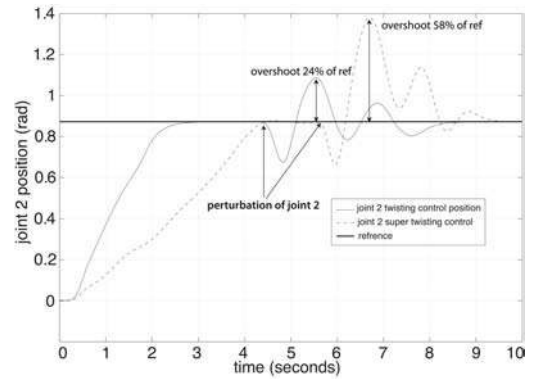


Fig. 10. Joint 2 *twisting* and *super twisting* laws (0.5Kg payload) with a perturbation for reference $(0.87, 1.39)^T \text{ rad}$

twisting law are respectively indicate in table V and VI.

twisting and *super twisting* controls manage to track the sinusoid, though a more important initial delay exists for the *super twisting* (Figs.11). Moreover the tracking error when using a *super twisting* is more important than that of a *twisting* law, particularly when a payload is carried.

TABLE V
TRACKING PARAMETERS OF
twisting LAW

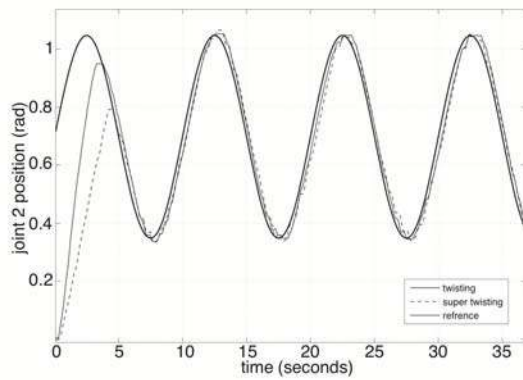
Joint	elbow (joint2)
A_M	2.41
A_m	2.1
U_M	5
$\%u_{eq}$	$0\% \cdot u_{eq}$

TABLE VI
TRACKING PARAMETERS OF
super twisting LAW

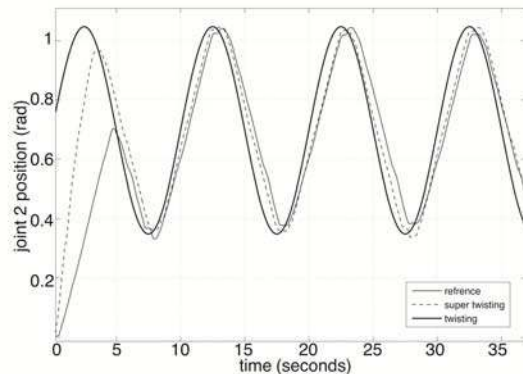
Joint	elbow (joint2)
α	0.1
ϵ_0	0.1
w	3
U_M	5
ρ	0.5
$\%u_{eq}$	$0\% \cdot u_{eq}$

VI. DISCUSSION AND CONCLUSIONS

The introduction of the equivalent control in the effective control proves to be useful if model uncertainty or parameter variations are not too far from the physical system. However, if this is not the case, the equivalent control will destabilize the system. As the joint 2 is a lot more sensitive to dynamics effects than the joint 1, the use of the equivalent control on this joint leads to instability of robot. On the contrary its use



(a) 0.1 hz without payload



(b) 0.1 hz with 0,5Kg payload

Fig. 11. *twisting* and *super twisting* in tracking a sinusoid

on the shoulder is beneficial. A payload of 0.5Kg is used to stress inertia and gravity effects.

The two controls of interest (*twisting* and *super twisting*) as practical controls are tested in regulation, versus a perturbation and in tracking a sinusoid. The *super twisting* law is too slow to present a practical interest. It is worth noting that a payload of 0.5Kg is used to stress the inertia and gravity effects. Both laws succeed in restabilising the system with, however the overshoot after perturbation represents 58% of the reference with the *super twisting* law, whereas it is only 24% with *twisting* law. Input sinusoid frequency is used 0.1 Hz with a payload variation of 0.5 Kg. both *twisting* and *super twisting* laws despite an initial delay manage to track the input signal. It is worth noting that a more important initial delay for the *super twisting* law.

As a first conclusion, the equivalent control shall not be used when the system model is not finely approximated, and only a discontinuous control is applied. In which case the response to 2-sliding controls becomes slow. This results confirm in part the outcome published [18]. It is thus necessary, in the future, to study the introduction of an additional term in order to reduce rising time and increase convergence speed toward the sliding surface. Also, it will be considered the relevance of the model improvements towards stability with the use of the equivalent control in the SMC.

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