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# Design of hybrid MoS<sub>2</sub>/photonic devices compatible with technological constraints

Jean-Baptiste Dory<sup>1,2</sup>, Olivier Gauthier-Lafaye<sup>2</sup>, Pascal Dubreuil<sup>2</sup>, Inès Massiot<sup>2</sup>, Stéphane Calvez<sup>2</sup>, Adnen Mlayah<sup>1,2</sup>

1. CEMES-CNRS, Université de Toulouse, Toulouse, France

2. LAAS-CNRS, Université de Toulouse, Toulouse, France

Corresponding authors : [amlayah@laas.fr](mailto:amlayah@laas.fr), [olivier.gauthier-lafaye@laas.fr](mailto:olivier.gauthier-lafaye@laas.fr)

## Abstract

The integration of transition metal dichalcogenide layers into photonic devices is a current challenge in the field of 2D materials. Based on numerical simulations, this work explores the design of devices combining an MoS<sub>2</sub> monolayer with planar photonic gratings sustaining localized optical resonances. A special attention is paid to the technological constraints. The optical response of six devices is compared taking into account the limitations imposed by the growth conditions of the MoS<sub>2</sub> layer and the processing of the resonant optical gratings. The reported photonic devices composed of grating filters and a backside reflector on silicon and silica substrates exhibit a theoretical absorption by the MoS<sub>2</sub> layer between 85 and 99% at 532 nm. The numerical simulations further show that the addition of an Al<sub>2</sub>O<sub>3</sub> encapsulation layer to protect the MoS<sub>2</sub> monolayer results in an increase of the performance of the devices. These hybrid MoS<sub>2</sub> based photonic devices are promising technological platforms for the study of the optical properties of integrated MoS<sub>2</sub> monolayers.

## 1. Introduction

Transition Metal Dichalcogenides (TMD) are two-dimensional (2D) semiconductor materials with astonishing physical properties [1] thanks to their stunning excitonic binding energy and valley spin properties [2]. Numerous works reported numerical simulations of devices achieving near perfect absorption by stacking these ultrathin dichalcogenide layers on or under metallic layers and antenna [3-12]. The devices with plasmonic structures on top of a TMD monolayer present the advantage of concentrating the electromagnetic field in the 2D material [13] paving the way for systems exploiting enhanced photoluminescence (PL) emission and/or photocurrent (PC) conversion. Thus, some works report measurements of significant PL enhancement of TMD monolayers in hybrid photonic devices with various metallic 2D structures near the TMD material [14-22]. However, the contact between the metal and the TMD material could be responsible for a quenching of TMD emission due to charge transfer [23-25]. To avoid this detrimental effect while keeping the ability to demonstrate exceptional absorption [26], the use of less common metals as Gallium [27], or stacked spacing layers [28] or only dielectric materials [29] have been reported.

A general review of the reported experimental demonstrations involving TMDs shows that the transition from isolated lab-scale objects to large-scale integrated devices comes with a significant degradation of the TMD material performances [30]. Given the recent demonstration of the synthesis of high-quality TMD monolayers on a wafer scale [31], one of the key challenges remaining to make TMD-based devices a reality is to develop integration methods compatible with TMD materials [1, 32]. Integration of TMD materials can be significantly improved by taking into account the technological and experimental constraints into the design of devices. As TMD materials show limited stability when exposed to air [33], an encapsulation layer is mandatory to protect the TMD material from contact with the atmosphere [34-38] or from detrimental subsequent technological steps. Similarly, should the

TMD material be deposited by CVD methods, the underlying multi-layer coated substrate has to withstand the high deposition temperature (above 400°C).

In this work, we investigate hybrid devices with a MoS<sub>2</sub> monolayer incorporated into grating based photonic cavities. The devices are designed to achieve a maximum optical absorption by the MoS<sub>2</sub> layer at a target excitation wavelength (532 nm in our case). The MoS<sub>2</sub> monolayer is integrated between a reflector and a resonant grating. The several stacks are conceived to protect the MoS<sub>2</sub> materials from degradation induced by the most reactive integration steps, in particular etching processes. Two types of resonant gratings are compared: an infinitely long grating-mode resonant filter (GMRF) and a more realistic cavity resonator integrated grating filter (CRIGF) with finite lateral dimensions. A CRIGF is composed of a grating coupler (GC) between two distributed Bragg reflectors (DBRs) on top of a waveguide layer [39]. Under optical illumination of the GC, a fraction of the incoming light is injected into a single-mode confined in the lateral cavity formed by the two DBRs. As demonstrated in [40], a CRIGF can be viewed as a small foot-print, folded GMRF device. Its small footprint is particularly interesting in the case of ultrathin 2D materials of which lateral size may be too small to allow an efficient coupling with a GMRF device. In this work, the MoS<sub>2</sub> monolayer is incorporated just below this waveguide resonator (Figure 1) leading to the absorption of the resonating optical mode by the MoS<sub>2</sub>.

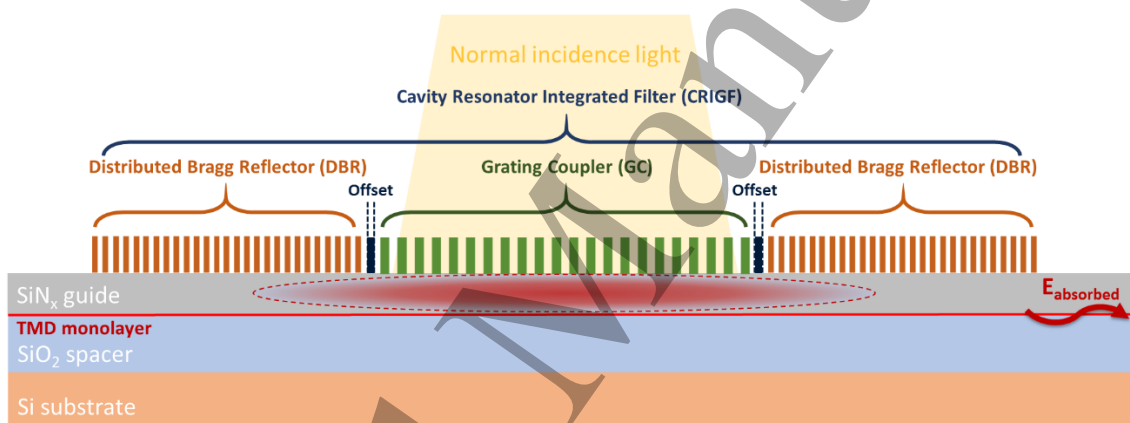


Figure 1: Schematic of the hybrid MoS<sub>2</sub>/photonic vertical stack with description of CRIGF grating parts. The device is designed to focus the incident light in the SiN<sub>x</sub> guiding layer. This configuration maximizes the absorption by the TMD monolayer directly below this guiding layer.

## 2. Numerical tools

Hybrid devices made of photonic structures and 2D materials combine micro and nanoscale engineering which, for modelling, implies microscopic meshing with locally sub-nanoscale precision. To maintain a reasonable calculation time, numerical simulations were performed using 2D-FMM methods [41] with an S-matrix algorithm [42]. The calculations are carried out using up to 1200 Fourier components for stacks with an entire CRIGF structure. For the CRIGF-based devices, the incoming light is under normal incidence with transverse electric (TE) polarisation; its intensity is Gaussian-shaped and overlaps only with the central part of the grating coupler. For GMRF-based devices, the calculations were performed for a plane wave at normal incidence, in TE polarization. The complex refractive index of the materials used in the simulations are provided in the Supplementary Information section. Absorption of the here considered dielectric materials (SiO<sub>2</sub>, SiN<sub>x</sub> and Al<sub>2</sub>O<sub>3</sub>) is negligible in the wavelength range of interest (500 to 800 nm). Thus, absorption occurs only within the MoS<sub>2</sub> layer and the Si substrate or back side reflector.

### 3. Discussion

#### 3.1. Optimal numerical solutions

For each investigated device, the geometrical parameters of the stack were optimized to maximize the absorbed fraction of the incident light. Table 1 summarizes these parameters and the calculated optical absorption by the MoS<sub>2</sub> layer integrated in the GMRF and CRIGF structures compared to a reference made of a MoS<sub>2</sub> layer on 90 nm SiO<sub>2</sub>/Si substrate (hereafter named MoS<sub>2</sub>/SiO<sub>2</sub>/Si).

Table 1 : Synthesis of geometrical parameters and calculated absorption performance of six studied devices compare to the theoretical optical response of MoS<sub>2</sub> monolayer on 90nm SiO<sub>2</sub>/Si substrate.

Grating type	SiN <sub>x</sub> grating				SiN <sub>x</sub> guide Thickness (nm)	Al <sub>2</sub> O <sub>3</sub> encapsulation Thickness (nm)	Absorption at 532nm (%)	SiO <sub>2</sub> spacer Thickness (nm)	Mirror	
	Thickness (nm)	Period (nm)	Filling factor	Offset factor					Material	T <sub>f</sub> (°C)
MoS <sub>2</sub> /SiO <sub>2</sub> /Si	---	---	---	---	---	---	20.9	90	Si bulk	1414
GMRF on Ag	135	294	0.50	---	125	---	99.1	250	Silver	961
GMRF on Al	110	292	0.50	---	130	---	97.6	225	Aluminium	660
GMRF on Si	120	298	0.50	---	110	---	85.8	250	Si bulk	1414
CRIGF on Si	120	298	0.50	1.00	110	---	82.0	250	Si bulk	1414
CRIGF with encapsulation	120	312	0.70	1.10	60	10	84.9	285	Si bulk	1414
Reversed CRIGF	60	288	0.45	1.05	120	20	89.1	210	Aluminium	660

Figure 2.a shows the investigated device consisting of a SiN<sub>x</sub> GMRF structure with a planar guiding layer on a monolayer MoS<sub>2</sub> onto a silicon oxide film with a backside metallic mirror forming a vertical cavity. Optimisation of the layer thicknesses and GMRF parameters (see Table 1) led to the selection of a particular structure that allows the absorption of 99.1% of the incident light at 532 nm in the MoS<sub>2</sub> monolayer as shown in Figure 2.c.

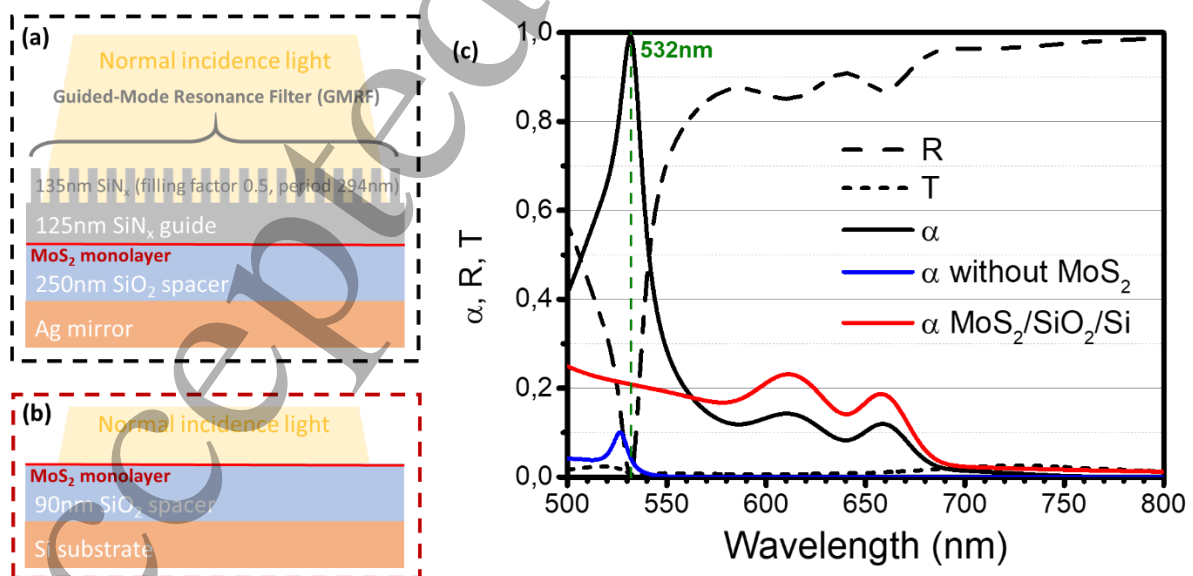


Figure 2: Schematics of GMRF/MoS<sub>2</sub> with Ag reflector vertical stacks (a), schematics of MoS<sub>2</sub>/SiO<sub>2</sub>/Si stack (b) and calculated optical response spectra of three devices (c): reflection, transmission and absorption fraction of energy calculated

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3 for GMRF/MoS<sub>2</sub> with Ag reflector device (black curves), absorption of the latter device without MoS<sub>2</sub> layer (blue curve) and  
4 absorption of standard MoS<sub>2</sub>/SiO<sub>2</sub>/Si stack (red curve).  
5

6 The near-perfect absorption at 532 nm is obtained owing to the coupling of the resonance of the  
7 GMRF structure with the B and C-exciton resonances of the MoS<sub>2</sub> layer. Indeed, the A and B exciton  
8 absorption bands are clearly visible around 660 and 610 nm, respectively; whereas the one of the C-  
9 exciton arises below 500nm [14, 43]. The absorption of the same device but without its MoS<sub>2</sub> layer is  
10 significantly lower. This residual absorption arises from the enhancement of the electromagnetic field  
11 near the GMRF structure and the absorption of the SiN<sub>x</sub> layer. Comparison of the GMRF/Ag reflector  
12 device with and without the MoS<sub>2</sub> layer shows that the MoS<sub>2</sub> layer absorbs the main part of the  
13 incident light (see the Supplementary Information). Since the experimental properties of MoS<sub>2</sub> are  
14 generally studied for flakes reported or grown on a 90nm SiO<sub>2</sub>/Si substrate (see Figure 2.b), we  
15 calculate that 20.9% of the incident light is absorbed in this reference stack at 532 nm, a value  
16 consistent with the results reported in the literature [44]. The GMRF with Ag reflector enhances the  
17 optical absorption by the MoS<sub>2</sub> layer by a factor 5 compared to the MoS<sub>2</sub>/SiO<sub>2</sub>/Si reference.  
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21 The GMRF-based structure on Ag reflector shows impressive performances, however its  
22 fabrication faces several technological challenges. Firstly, SiN<sub>x</sub> film is commonly grown using plasma  
23 assisted processes under reactive conditions (nitride atmosphere and/or nitride precursors) which may  
24 create defects in the atomic structure of the TMD layer during the early stages of the deposition.  
25 Secondly, silver (back reflector) is rarely used in microelectronic devices, because of its low thermal  
26 stability incompatible with the MoS<sub>2</sub> deposition temperature. The melting temperature of the material  
27 used as back reflector is given in the Table 1 as an indication of its thermal stability. One must keep in  
28 mind that degradation of the reflector (delamination, phase segregation,...) occurs at temperatures  
29 way below its melting temperature. The incompatibility between the low thermal stability of silver and  
30 the MoS<sub>2</sub> deposition temperature can only be solved using a transfer of the MoS<sub>2</sub> layer or by deposition  
31 of the Ag layer, after the growth of the MoS<sub>2</sub> layer, combined with a challenging back side thinning  
32 down to the spacer layer. Vertical DBRs based on dielectric materials are a potential substitute to  
33 metallic reflector. However, their fabrication requires an excellent repeatability (in composition and  
34 thickness) of dielectric deposition steps and the multiplicity of layers which can be a source of stack  
35 delamination.  
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39 To bypass these technological issues, alternative structures need to be explored and compared to  
40 the GMRF based near-perfect absorber structure. Furthermore, the sharp resonance generated in the  
41 hybrid photonic device is well adapted to the illumination by spectrally coherent light sources, which  
42 can be focused to the active region of the device. To this aim, CRIGF structures, consisting of a resonant  
43 grating of finite length and an additional lateral optical confinement have been shown to facilitate  
44 high-Q cavity operation under focused laser spot [45]. As such, CRIGFs are also more amenable to lead  
45 to high performance devices with a spatially-restricted uniformity.  
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### 49 **3.2. Alternative devices based on practical integration considerations**

50 In this work, the GC of the CRIGF structures is composed of 41 periods matching a beam width of  
51 about 12 μm. As the period of the DBRs is half the GC period, considering DBRs composed of 100  
52 periods, the total width of the device is 45 μm at maximum. Figure 3.a shows the theoretical optical  
53 response of three types of hybrid CRIGF/MoS<sub>2</sub> devices.  
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56 The first CRIGF/MoS<sub>2</sub>-based design is similar to the previously studied GMRF/MoS<sub>2</sub> design (see  
57 Figure 2.a) with the GMRF structure and Ag mirror replaced respectively by a CRIGF structure and a Si  
58 substrate (see Figure 3.b). As reported in Table 1, the Ag mirror improves significantly the absorption  
59 by the MoS<sub>2</sub> layer compared to the same device on a standard silicon substrate (99.1 compared to  
60



85.8%). However, the stack on Si substrate is compatible with the direct deposition of TMD materials at high temperature (around 650°C). With the CRIGF structure, the absorption by the TMD layer is weaker than with a GMRF structure (82.0 instead of 85.8%). This is due to the finite lateral size of the CRIGF. Indeed, for a GMRF limited to 41 periods (as the GC part of the CRIGF) and using an illumination source with the same gaussian beam waist, the theoretical absorption by the MoS<sub>2</sub> layer in the GMRF decreases to 80.8% (as compared to the initial 85.8%). Thus, when considering realistic lateral dimensions of the GMRF structure, better performances are predicted for the CRIGF structure compared to the GMRF.

The second CRIGF design (see Figure 3.c) is composed of an additional alumina Al<sub>2</sub>O<sub>3</sub> layer intercalated between the MoS<sub>2</sub> monolayer layer and the SiN<sub>x</sub> guide. The Al<sub>2</sub>O<sub>3</sub> layer is a protective capping layer which could be deposited to prevent contamination and degradation of the MoS<sub>2</sub> layer during the reactive processes. Indeed, Al<sub>2</sub>O<sub>3</sub> is airtight and has a good chemical stability. In addition, Al<sub>2</sub>O<sub>3</sub> is commonly obtained by atomic layer deposition (ALD), a softer process compared to chemical or physical vapour deposition (CVD or PVD). With a 10 nm thick Al<sub>2</sub>O<sub>3</sub> layer and optimized parameters of the CRIGF (see values in Table 1), the maximum of absorption by the MoS<sub>2</sub> layer reaches 84.9% due to a better confinement of the optical mode at 532 nm. Hence, the protective Al<sub>2</sub>O<sub>3</sub> integrated in the CRIGF/MoS<sub>2</sub> device is beneficial as it increases the achievable maximum of absorption by the MoS<sub>2</sub> layer.

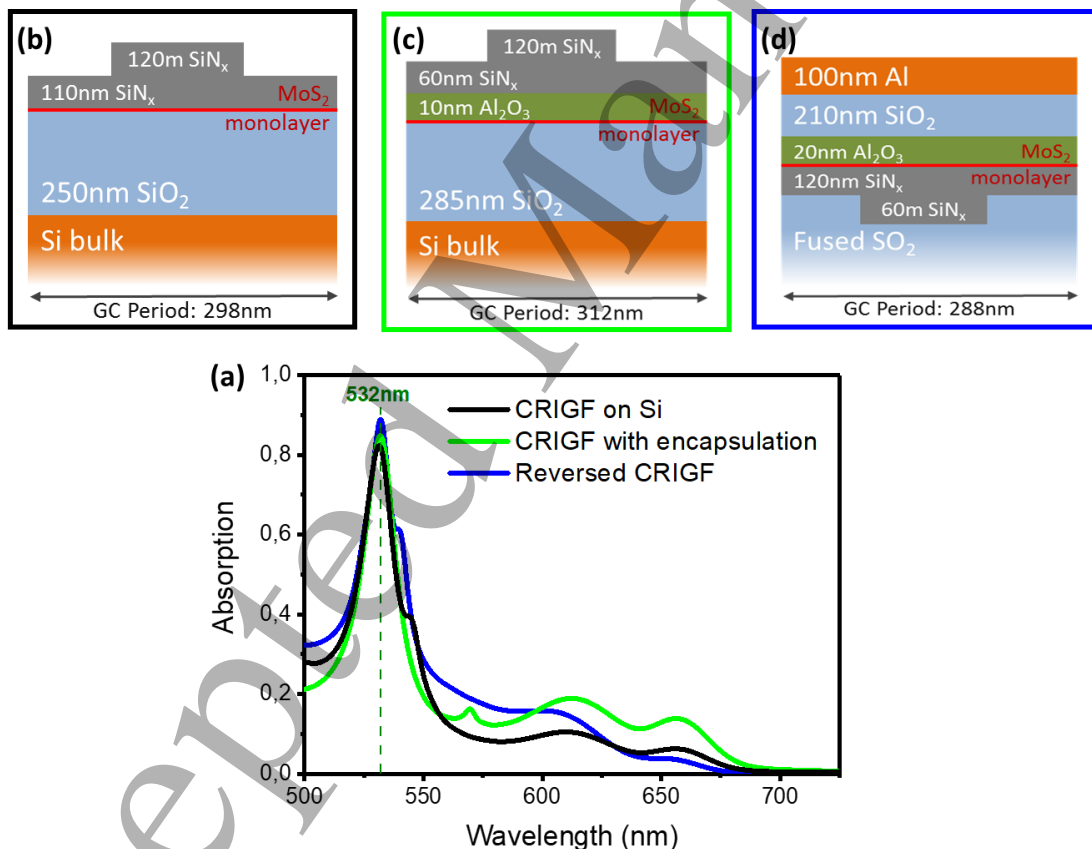


Figure 3: Schematics of the vertical stack and calculated optical response spectra of three hybrid CRIGF/MoS<sub>2</sub> structures: CRIGF on Si (b, black), CRIGF with encapsulation (c, green) and reversed CRIGF (d, blue).

Finally, a third CRIGF-based design is considered (Figure 3.d). It involves an inverted fabrication process flow allowing the integration of a metal mirror after the growth of the MoS<sub>2</sub> layer. In this way, the metal is kept below its melting temperature which can be close to the MoS<sub>2</sub> growth temperature (650°C) in the case of Aluminium for example. This reversed design is based on a transparent fused

silica substrate which permits a back side optical excitation. After partial etching of the substrate to fabricate the CRIGF structure, the corrugated substrate is covered by  $\text{SiN}_x$ . The  $\text{MoS}_2$  layer would then be grown onto the  $\text{SiN}_x$  and almost no change in the nucleation and growth of the 2D material are expected compared to  $\text{SiO}_2$  substrate as both dielectrics are amorphous materials. Because of the inversion in the integration steps, the protective  $\text{Al}_2\text{O}_3$  layer is incorporated between the  $\text{MoS}_2$  layer and the  $\text{SiO}_2$  spacer. In this reversed CRIGF-based design, the encapsulation of the  $\text{MoS}_2$  layer is essential as the oxidizing conditions under which the  $\text{SiO}_2$  is deposited may damage the  $\text{MoS}_2$  and introduce defects that strongly alter its optical absorption and emission properties. Finally, an aluminium reflector is added on the top of the device. Despite its slightly lower reflectance at 532 nm, Aluminium is preferred to silver due to its better thermal stability (see Table 1). According to the calculations with the reversed CRIGF-based design, the optical absorption by the  $\text{MoS}_2$  layer reaches 89.1% at 532 nm. The integration of emerging 2D compounds in 3D devices is challenging considering the potential detrimental impact of the integration processes on the performances of the TMD materials [30]. The latter device anticipates several potential technological fabrication limitations while exhibiting impressive absorption as compared to the other CRIGF devices investigated in this work.

## 4. Conclusion

In summary, using numerical simulations, we found that the integration of a 2D  $\text{MoS}_2$  layer between a CRIGF or GMRF structure and a reflector enhances the optical absorption by the  $\text{MoS}_2$  layer to 85 to 99% as compared to the  $\approx 20\%$  achieved with the standard  $\text{MoS}_2/90$  nm  $\text{SiO}_2/\text{Si}$  stack. The increase is mainly due to the coupling of the resonance sustained by the CRIGF or the GMRF with the  $\text{MoS}_2$  excitonic absorption. The calculated absorption by the  $\text{MoS}_2$  layer implemented in the CRIGF-based device is higher than the one reached with the GMRF-based device. Furthermore, the substitution of the Si substrate by an aluminium back reflector and the addition of a capping layer increase the theoretical absorption by the  $\text{MoS}_2$ . The designed devices are compatible with the material thermal and chemical constraints and technological processes and their optical response is suitable for studying the optical properties of integrated  $\text{MoS}_2$  monolayers. This investigation of hybrid TMD/photonic devices is a contribution to the understanding of the impact of integration processes on TMD materials, identified as the main current challenge preventing an ubiquitous use of 2D TMD materials [1, 30].

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